

A Wideband Dipole Array for Directed Energy Applications and Digital TV Reception

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**33rd Annual
Antenna Applications Symposium
September 23, 2009**

Report Documentation Page			Form Approved OMB No. 0704-0188	
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1. REPORT DATE 23 SEP 2009	2. REPORT TYPE	3. DATES COVERED 00-00-2009 to 00-00-2009		
4. TITLE AND SUBTITLE A Wideband Dipole Array for Directed Energy Applications and Digital TV Reception			5a. CONTRACT NUMBER	
			5b. GRANT NUMBER	
			5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S)			5d. PROJECT NUMBER	
			5e. TASK NUMBER	
			5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Physical Sciences Inc,20 New England Business Center,Andover,MA,01810			8. PERFORMING ORGANIZATION REPORT NUMBER	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)			10. SPONSOR/MONITOR'S ACRONYM(S)	
			11. SPONSOR/MONITOR'S REPORT NUMBER(S)	
12. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution unlimited				
13. SUPPLEMENTARY NOTES				
14. ABSTRACT				
15. SUBJECT TERMS				
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT Same as Report (SAR)	18. NUMBER OF PAGES 26
a. REPORT unclassified	b. ABSTRACT unclassified	c. THIS PAGE unclassified	19a. NAME OF RESPONSIBLE PERSON	

Outline

- **Problem and motivation**
- **The “ribcage” dipole antenna**
- **Comparisons with classic configurations**
- **Ribcage dipole antenna for communications**
 - Optimized ribcage dipole with balun
 - Simulations and laboratory measurements
- **Antenna array for Directed Energy applications**
 - Optimized unit cell with balun
 - Customized power dividers
 - 8x8 array of ribcages: simulations and preliminary laboratory tests
 - Composite array model for antenna array pattern modeling
- **Conclusions and future work**

Compact High Performance RF Communications

Motivation #1



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Whip antennas for HF communications

- Simple classic design
- Narrow bandwidth
- High visibility
- Needs assembly for portability

Ribcage dipole antenna

- Low profile
- Excellent performance over a ground plane
- Wide impedance bandwidth
- Uniform antenna pattern over the bandwidth
- Needs further development and funds

Phase II Army SBIR Contract #: W15QKN-08-C-0493, TPOC; Keith Braun, ARMY – AMSML - PICATINNY

Compact Portable Focused Beam Antenna

Motivation #2

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Parabolic dish antennas

- Wide band
- High gain
- Focused beam
- Simple feeding
- Complex position control
- Large volume
- Not easily portable
- Highly visible

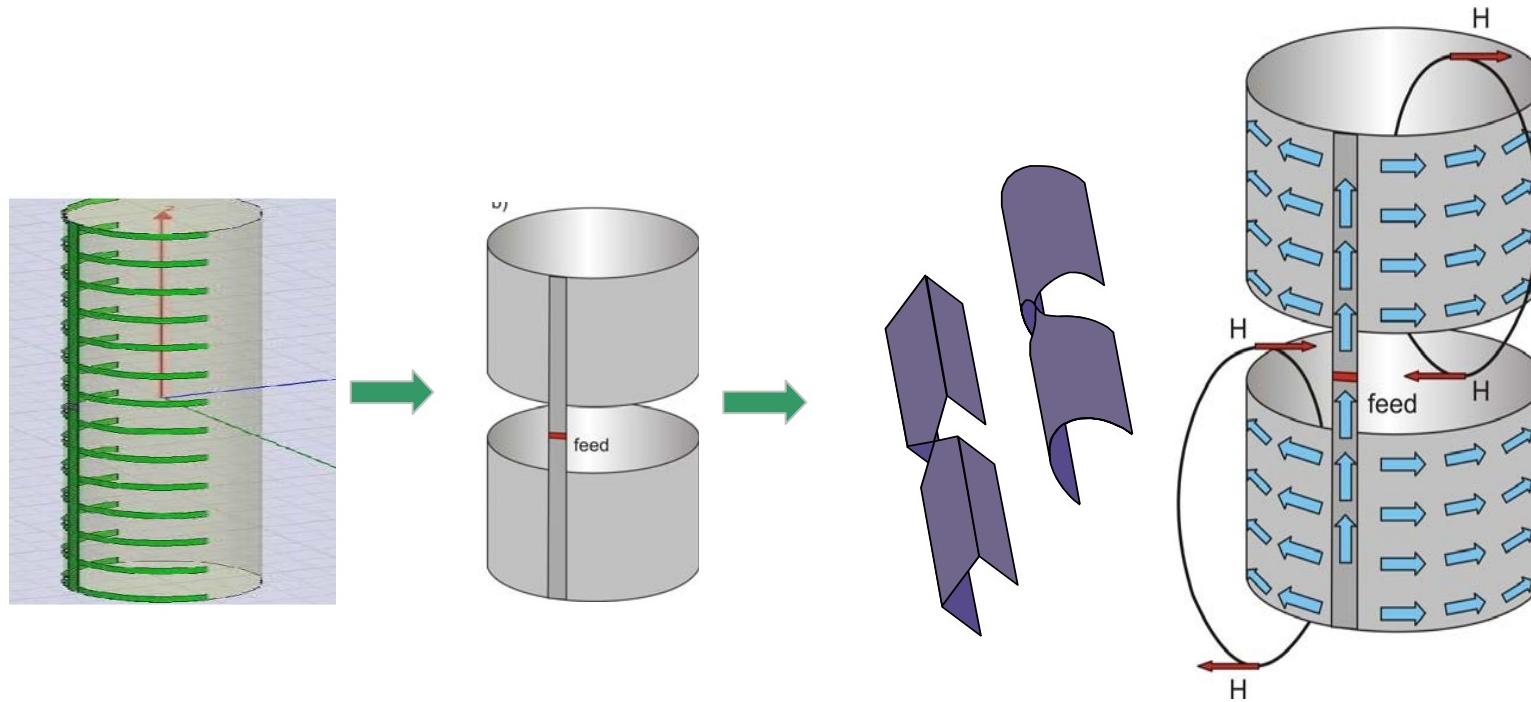
Antenna array of ribcage elements

- Wide-band, high gain, narrow beam
- Possibility of electronic scanning
- Compact, low-profile, easily portable
- Can be stowed in sub-array modules
- More complex feeding network

The Origins of the “Ribcage” Dipole

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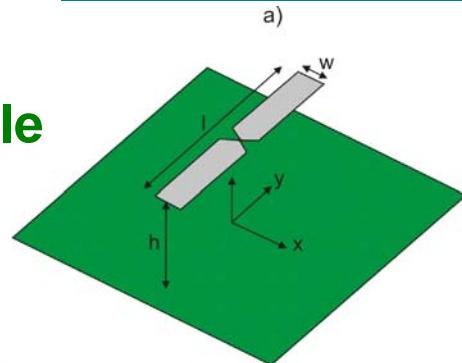
- **Volumetric dipole antenna with ribs, wings, or sleeves**
- **Closed ring or open sleeve**
- **Intrinsic additional magnetic field**



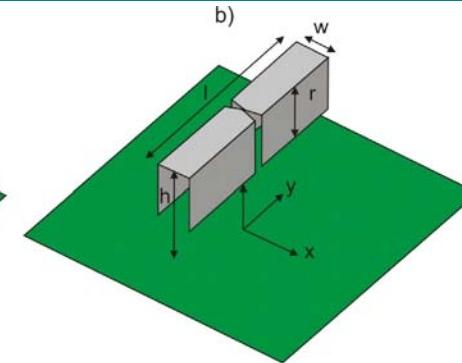
Wideband Volumetric Antenna: Dipole With Sleeves

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Blade Dipole

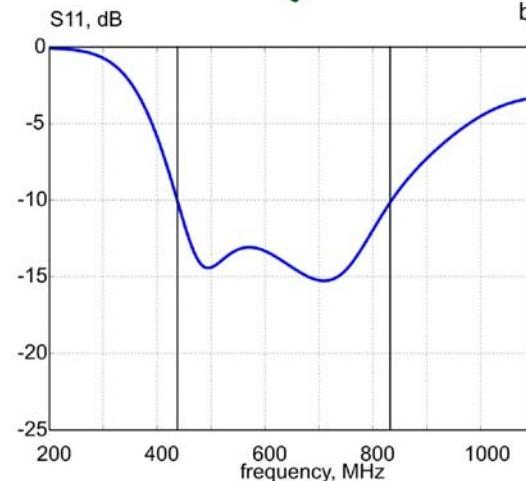
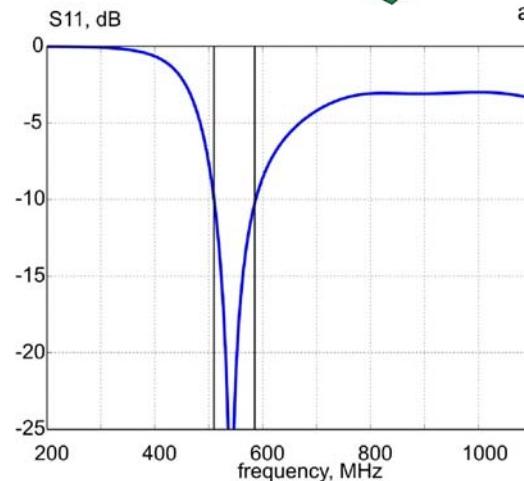


a)



b)

Ribcage Dipole

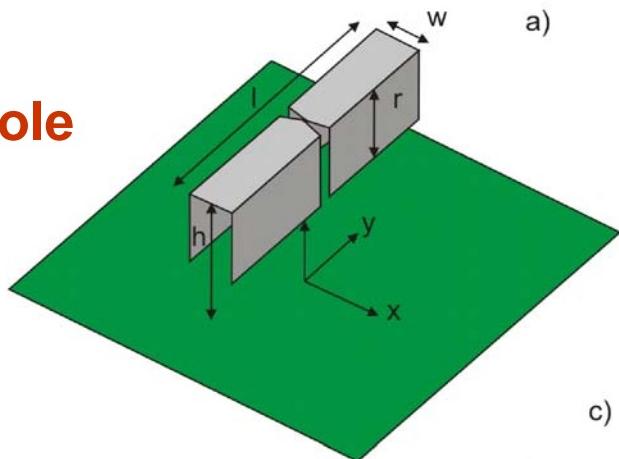


The **ribcage dipole** has wider bandwidth than **blade dipole** of same width and length.

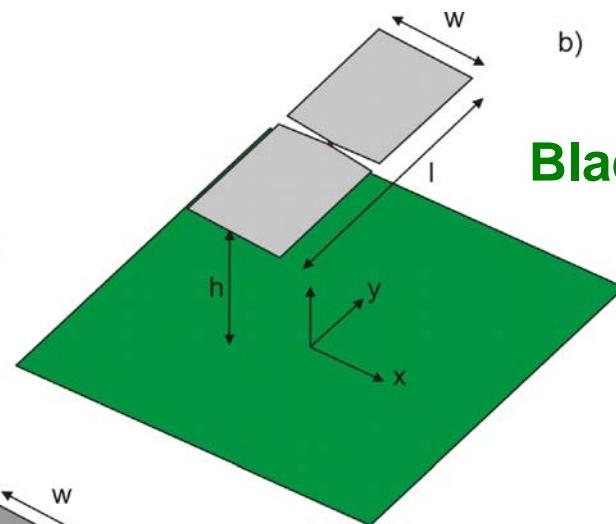
Antenna	Height above Ground Plane	Width	Total Length	(Sleeve) Depth	Ground Plane
Blade dipole	h=105 mm	w=30 mm	l=220 mm	NA	300×300 mm
Ribcage dipole	h=160 mm	w=30 mm	l=220 mm	r = 70 mm	300×300 mm

Comparison of Dipoles Over Ground Plane

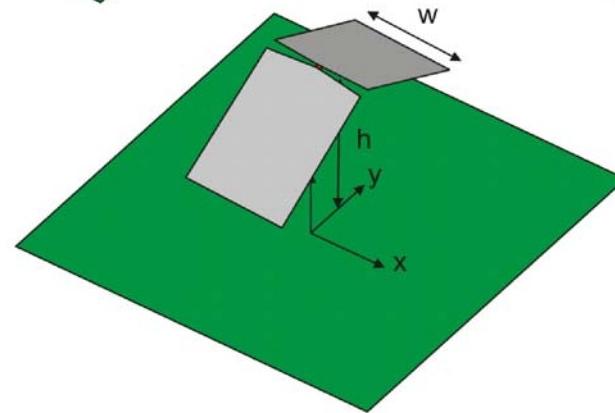
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Ribcage Dipole

a)

Blade Dipole

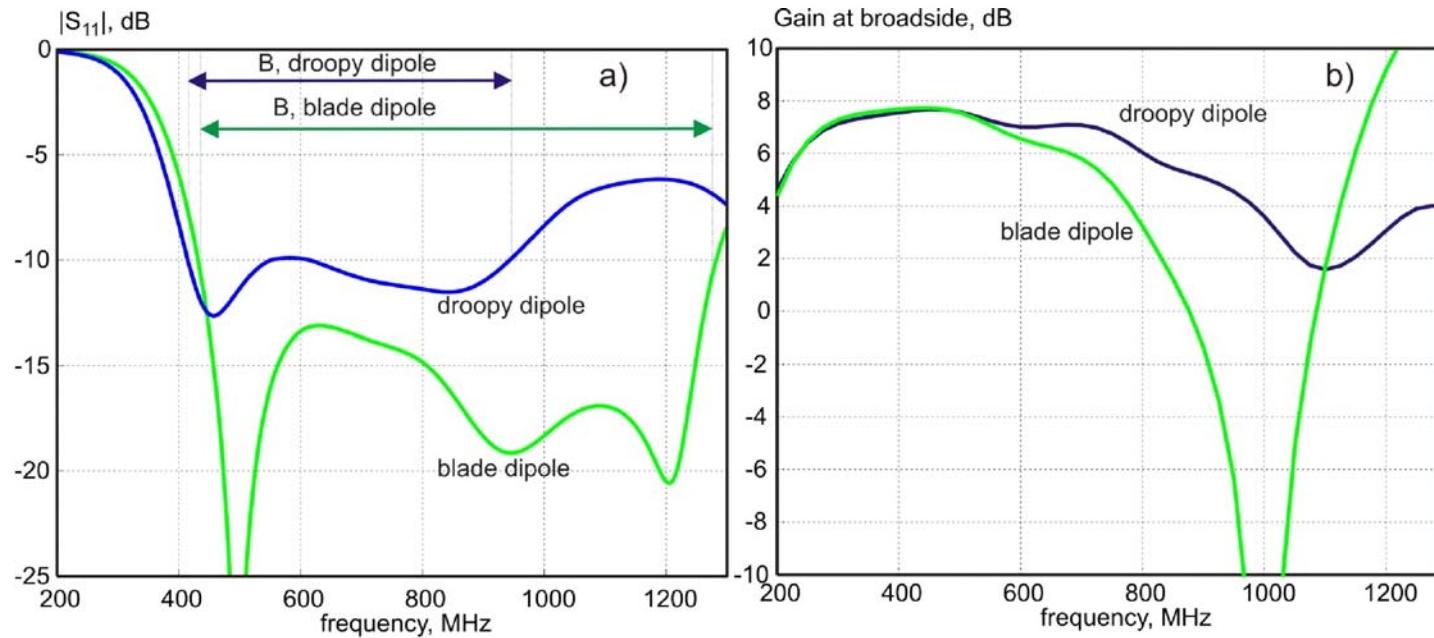
b)

**Droopy Dipole**

Optimized Droopy Dipole and Blade Dipole

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Antenna	Height over Ground Plane	Width	Total Length	Sleeve Depth	GP
Blade dipole	$h=150$ mm	$w=120$ mm	$l=220$ mm	NA	300×300 mm
Droopy dipole	$h=150$ mm	$w=140$ mm	$l=220$ mm	NA	300×300 mm

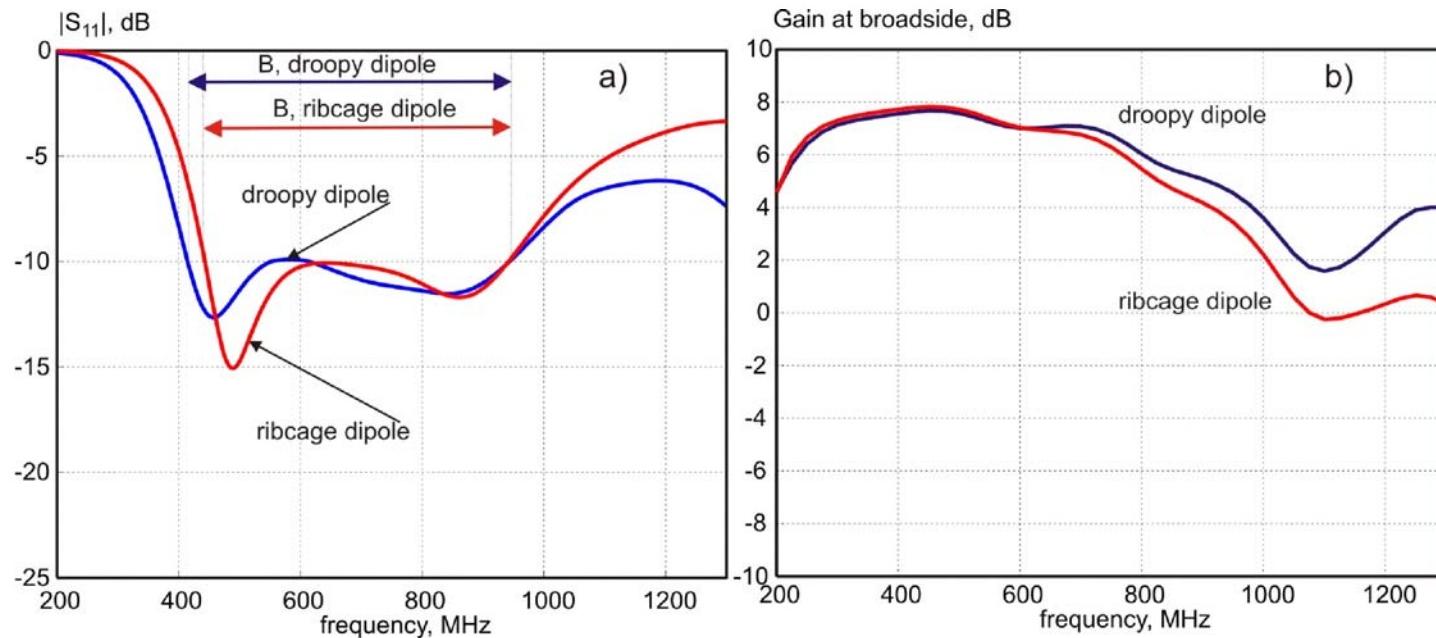


- The **blade dipole** has a wider impedance bandwidth
- The **droopy dipole** has a more uniform gain over the bandwidth

Ribcage Dipole and Droopy Dipole

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Antenna	Height from Ground Plane	Width	Length	Sleeve Depth	GP
Ribcage dipole	h=150 mm	w=25 mm	l=220 mm	60mm	300x300 mm
Droopy dipole	h=150 mm	w=140 mm	l=220 mm	NA	300x300 mm



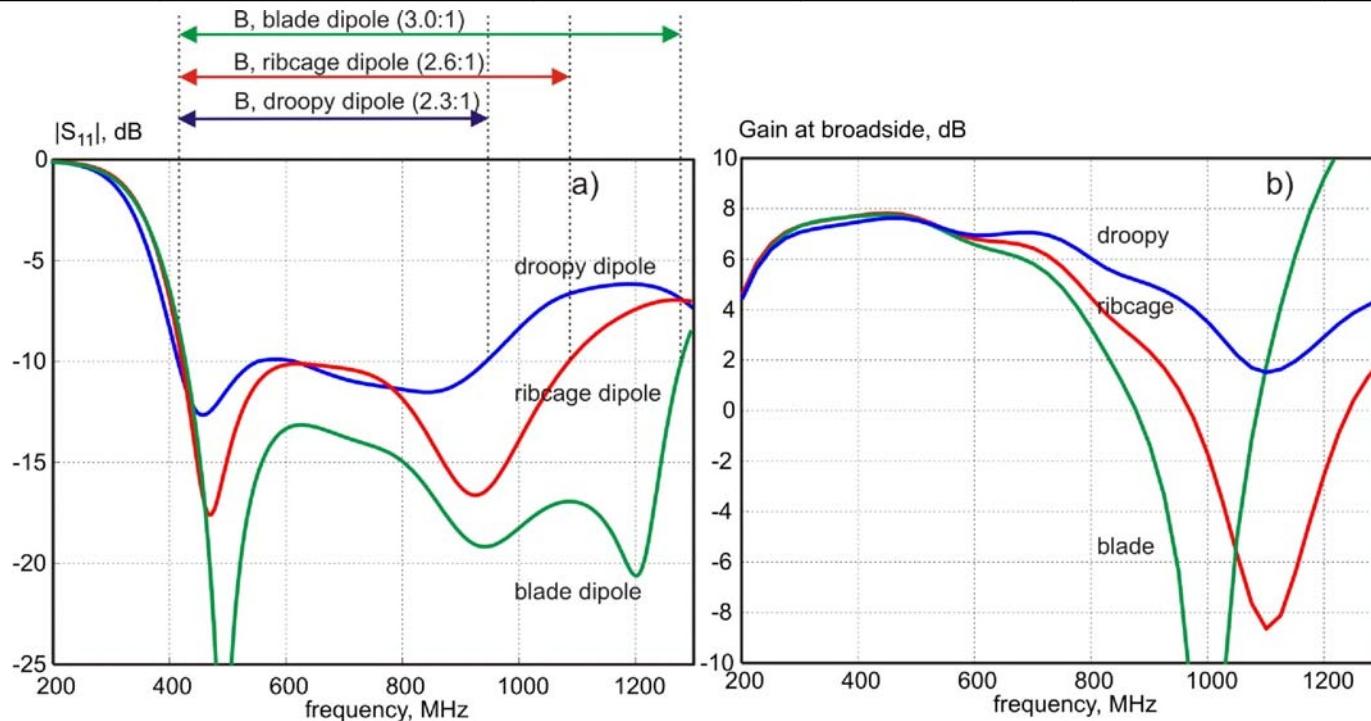
- The ribcage dipole can be designed to have similar performance than the droopy dipole

Ribcage Dipole:

Between Droopy Dipole and Blade Dipole

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Antenna	Height From Ground Plane	Width	Length	Sleeve Depth	GP
Ribcage dipole	$h=150$ mm	$w=55$ mm	$l=220$ mm	40 mm	300×300 mm
Droopy dipole	$h=150$ mm	$w=140$ mm	$l=220$ mm	NA	300×300 mm
Blade dipole	$h=150$ mm	$w=120$ mm	$l=220$ mm	NA	300×300 mm

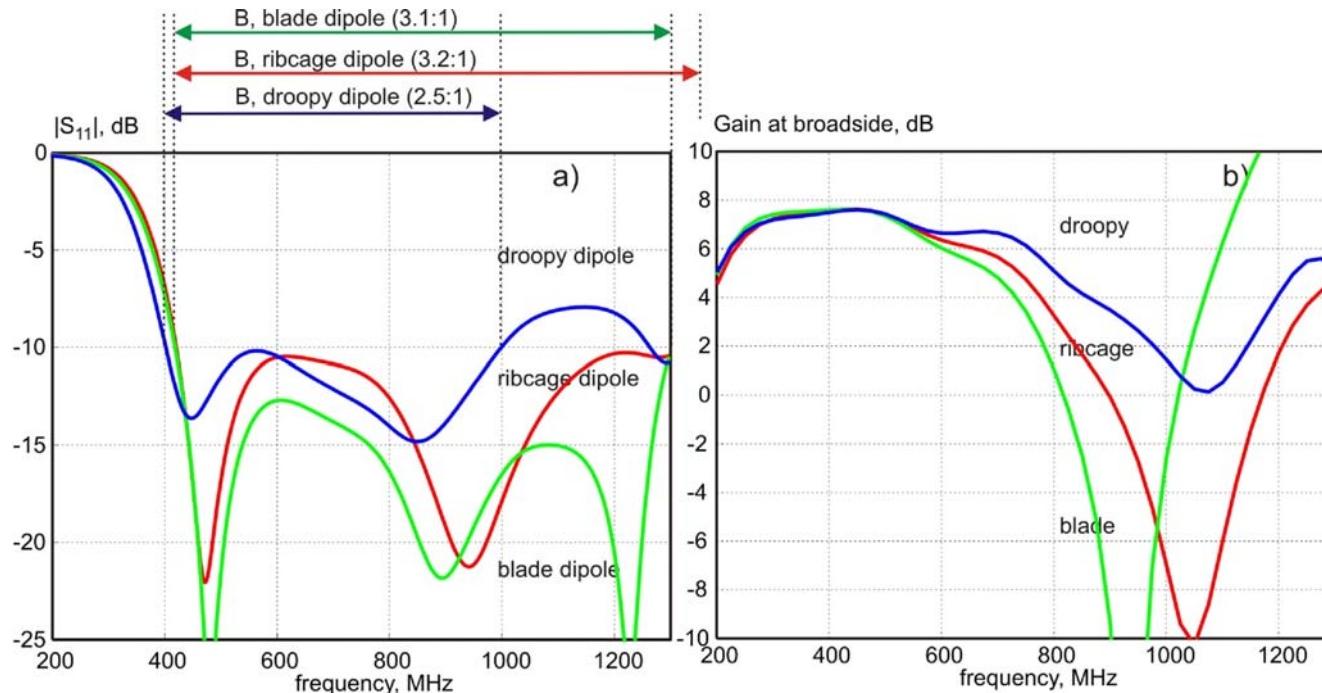


- The ribcage dipole can be designed to combine advantages of both droopy dipole and blade dipole (its extreme cases).

Optimized Ribcage Dipole

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Antenna	Height from Ground Plane	Width	Length	Sleeve Depth	GP
Ribcage dipole	$h=160\text{mm}$	$w=50\text{mm}$	$l=220\text{mm}$	40mm	$300\times300\text{mm}$
Droopy-blade dipole	$h=160\text{mm}$	$w=140\text{mm}$	$l=220\text{mm}$	NA	$300\times300\text{mm}$
Wide-Blade dipole	$h=160\text{mm}$	$w=120\text{mm}$	$l=220\text{mm}$	NA	$300\times300\text{mm}$

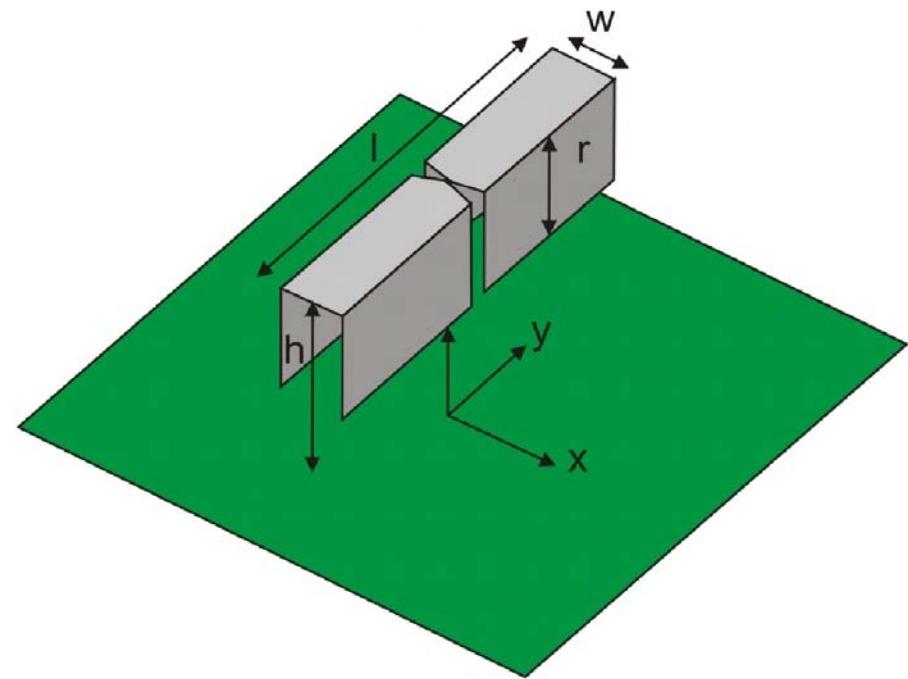


- A **ribcage dipole** can be optimized to have wider impedance bandwidth than a **droopy dipole** and better gain bandwidth than a **blade dipole**

Advantages of Ribcage Dipoles

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- Space optimization
- Design flexibility (more parameters)
- Wide impedance bandwidth
- Wide gain bandwidth

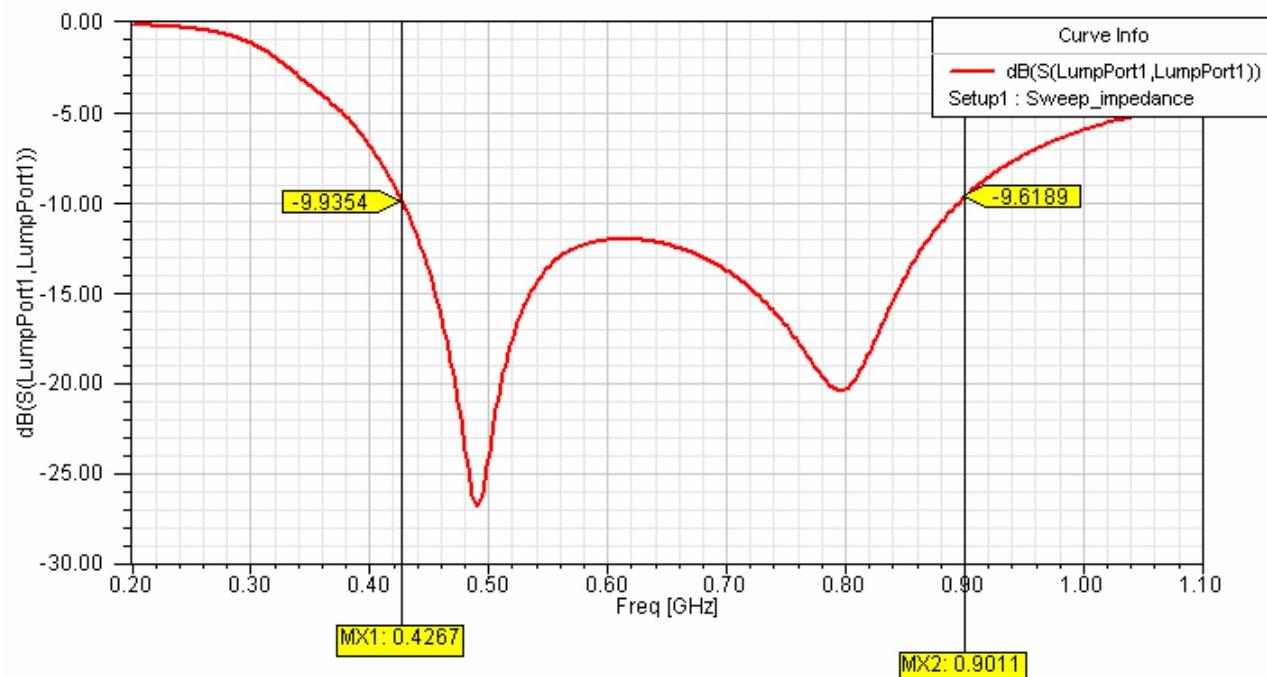
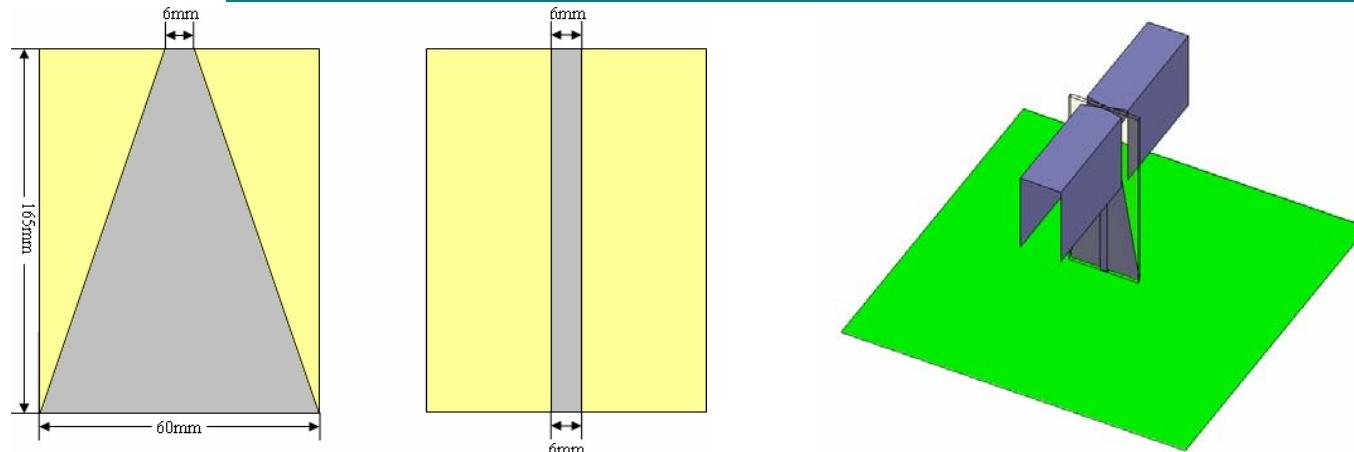




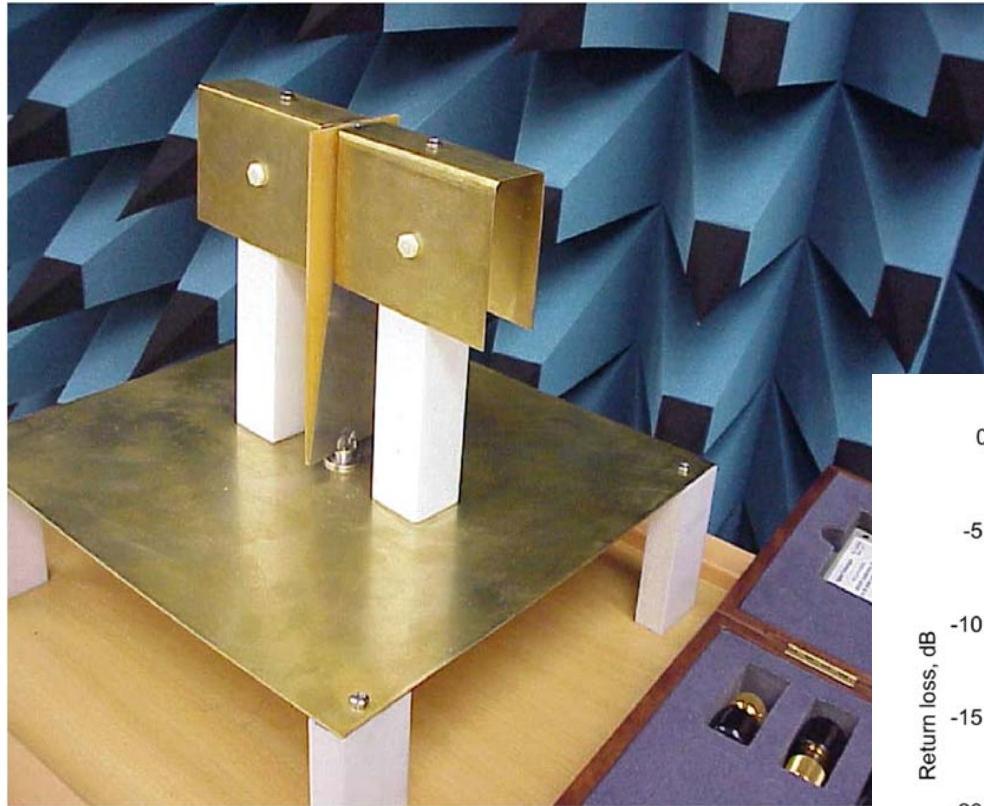
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Ribcage Antenna With Tapered Balun

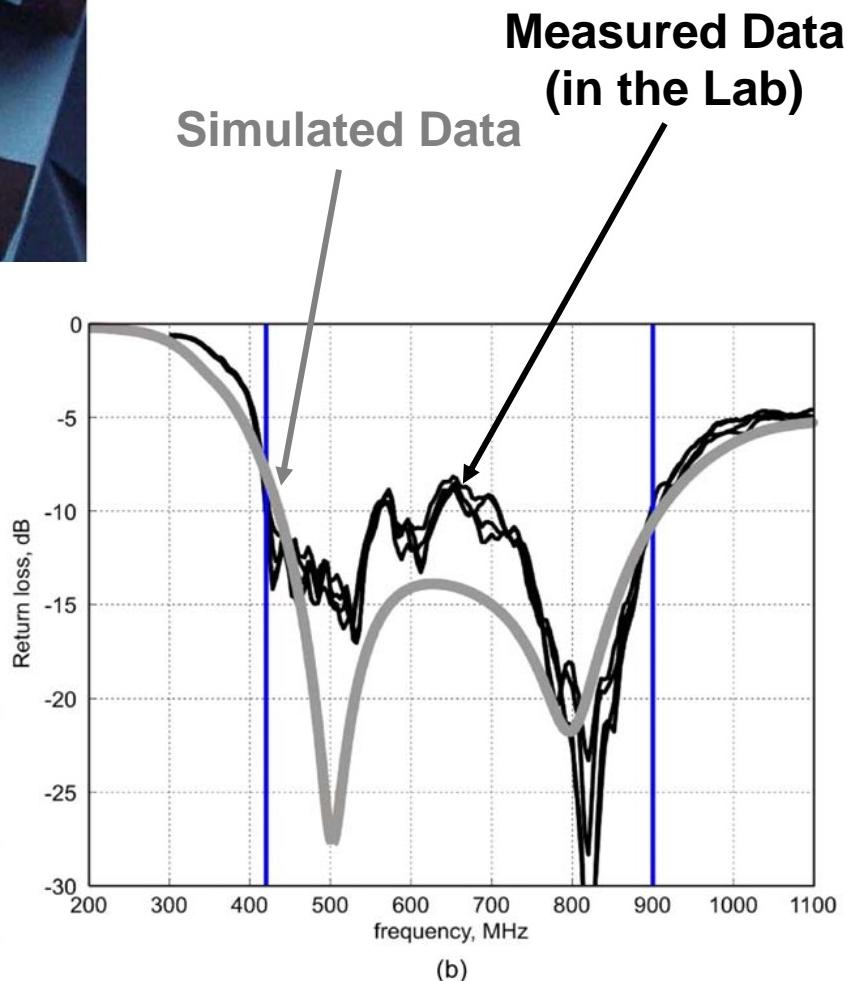
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Ribcage Antenna With Balun and Teflon Support



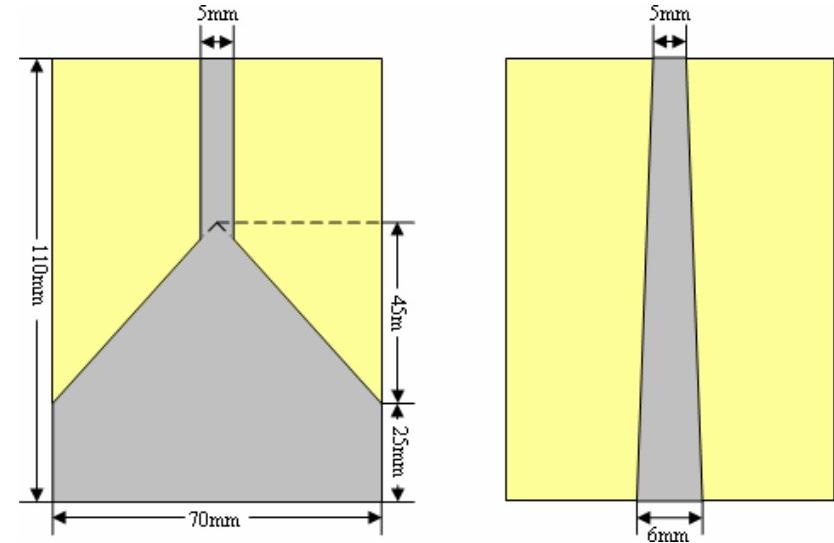
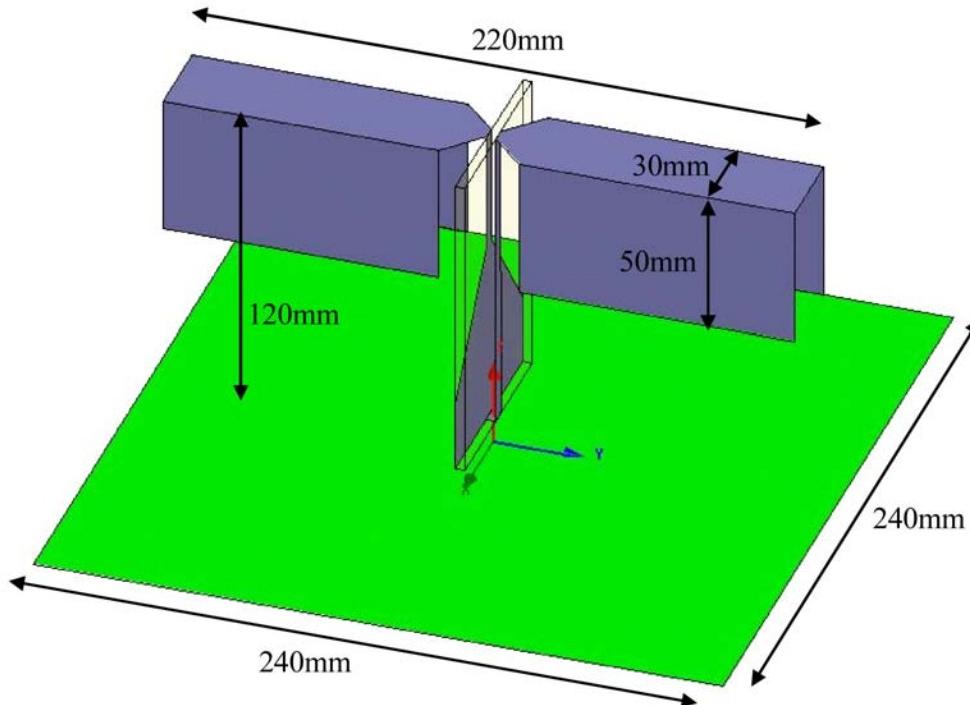
Height from Ground Plane	Width	Total Length	Sleeve Depth	GP
$h=175$ mm	$w=35$ mm	$L=210$ mm	$r=70$ mm	300×300 mm



Optimized Unit Cell With Balun

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- Optimized single radiating element for the array

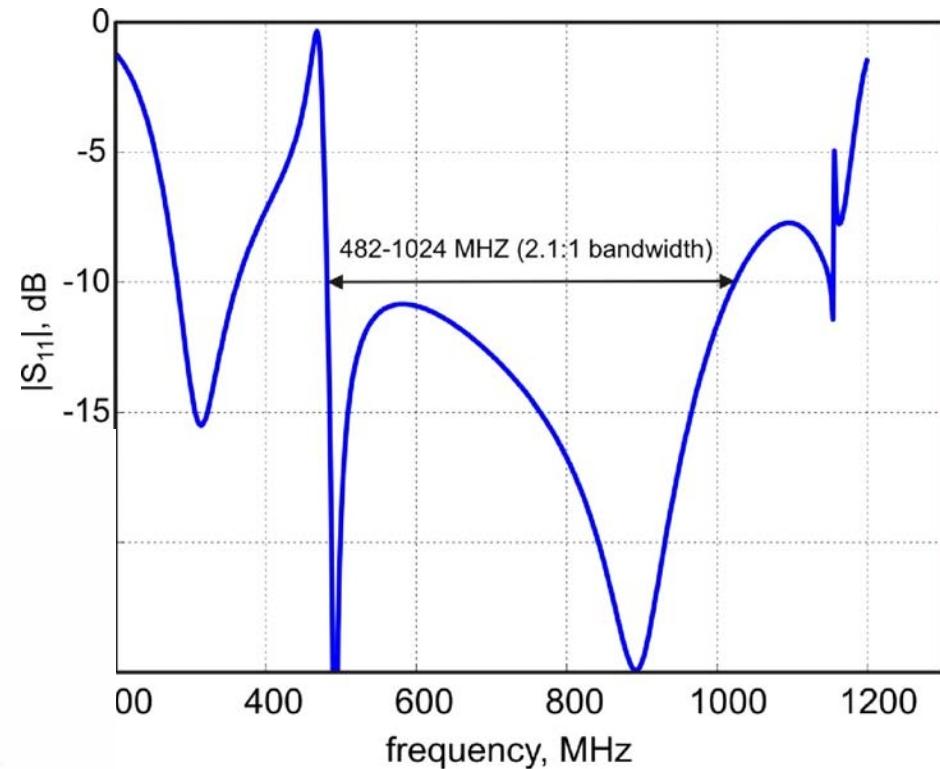
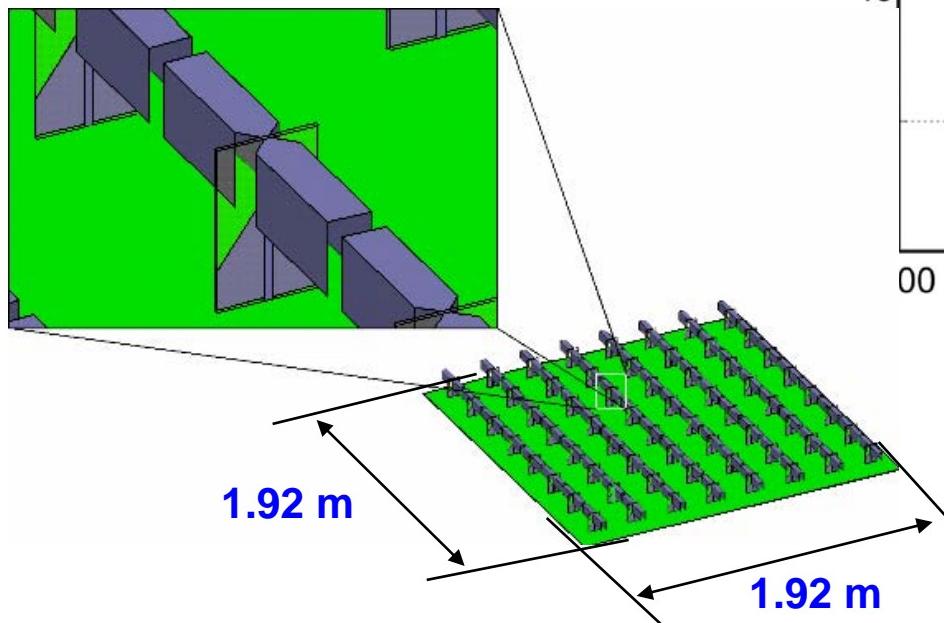


- Optimized tapered balun for the array configuration

Simulated Antenna Array Return Loss

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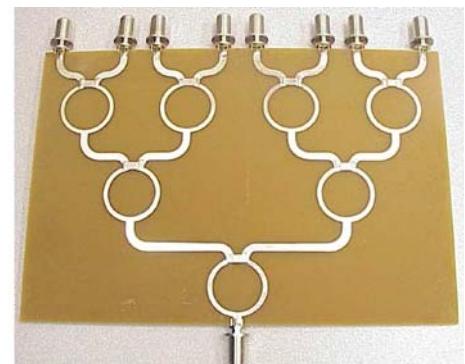
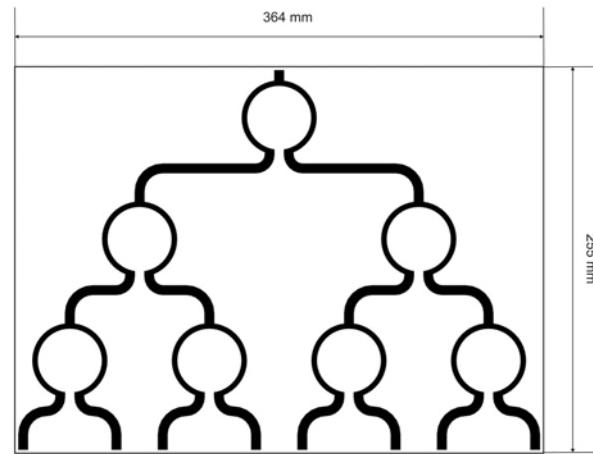
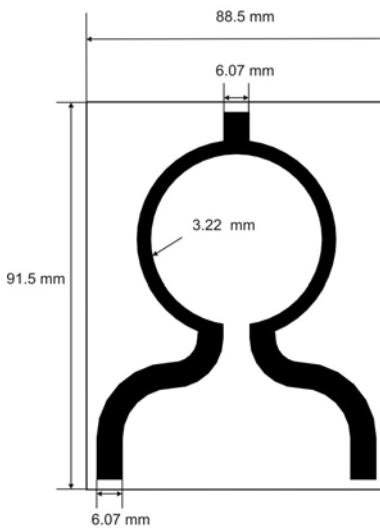
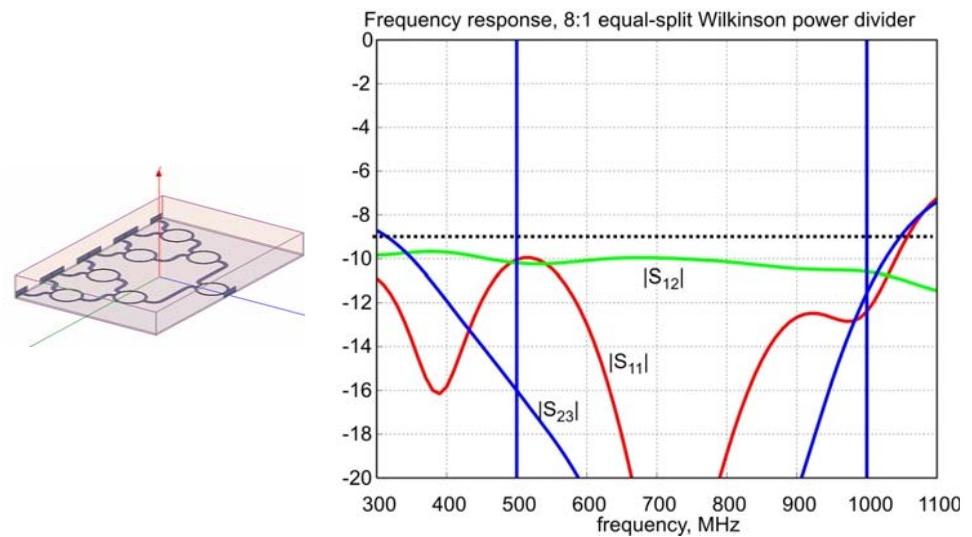
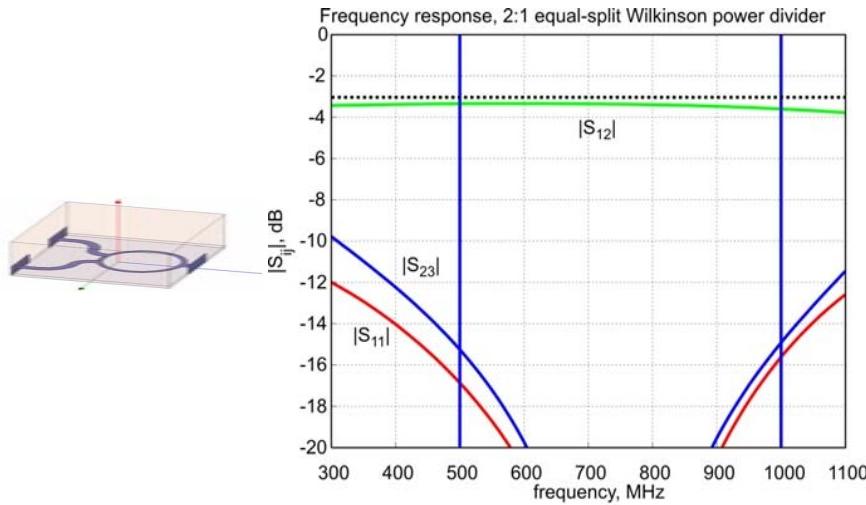
- Return Loss for an infinite antenna array of ribcages with tapered balun

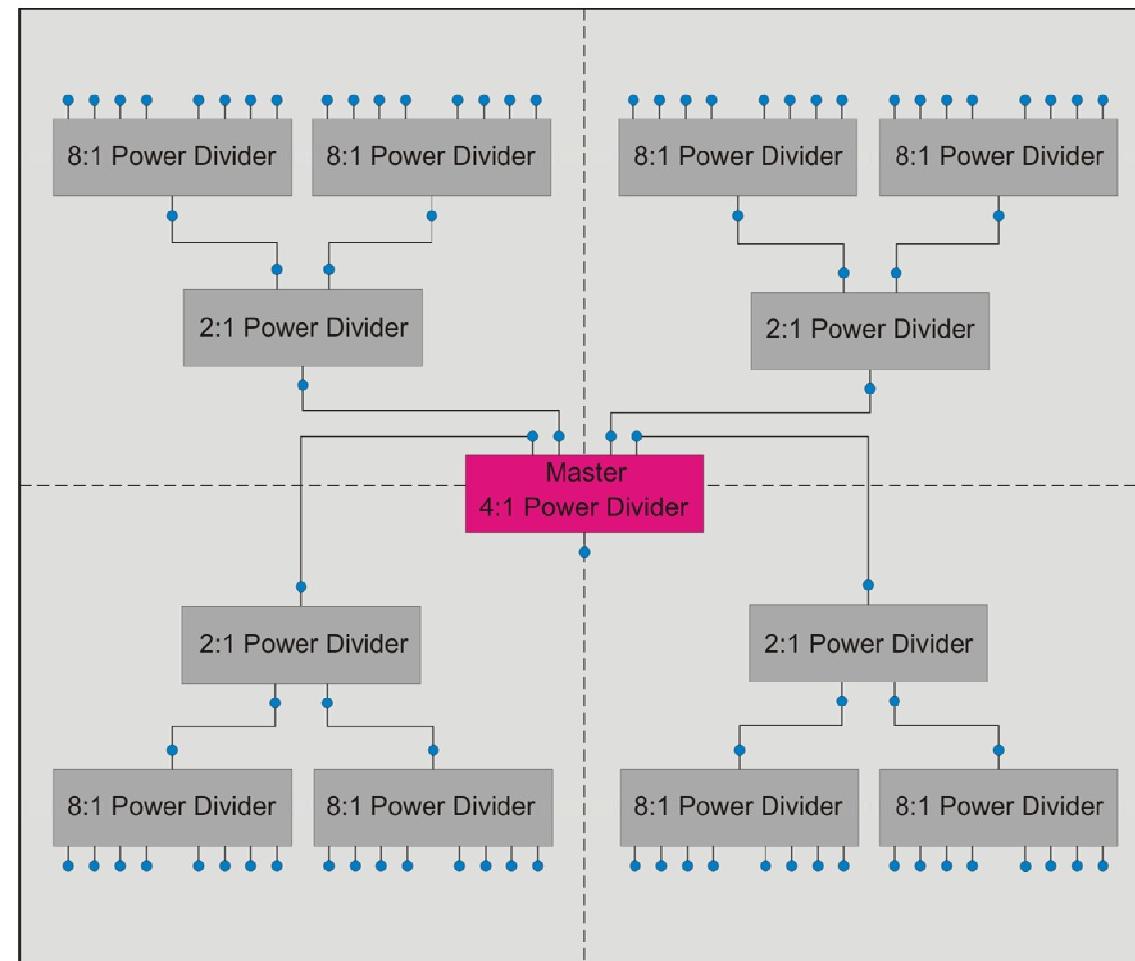


- 1.92 x 1.92 m (8x8) array
- Equivalent to a 3 m parabolic reflector antenna

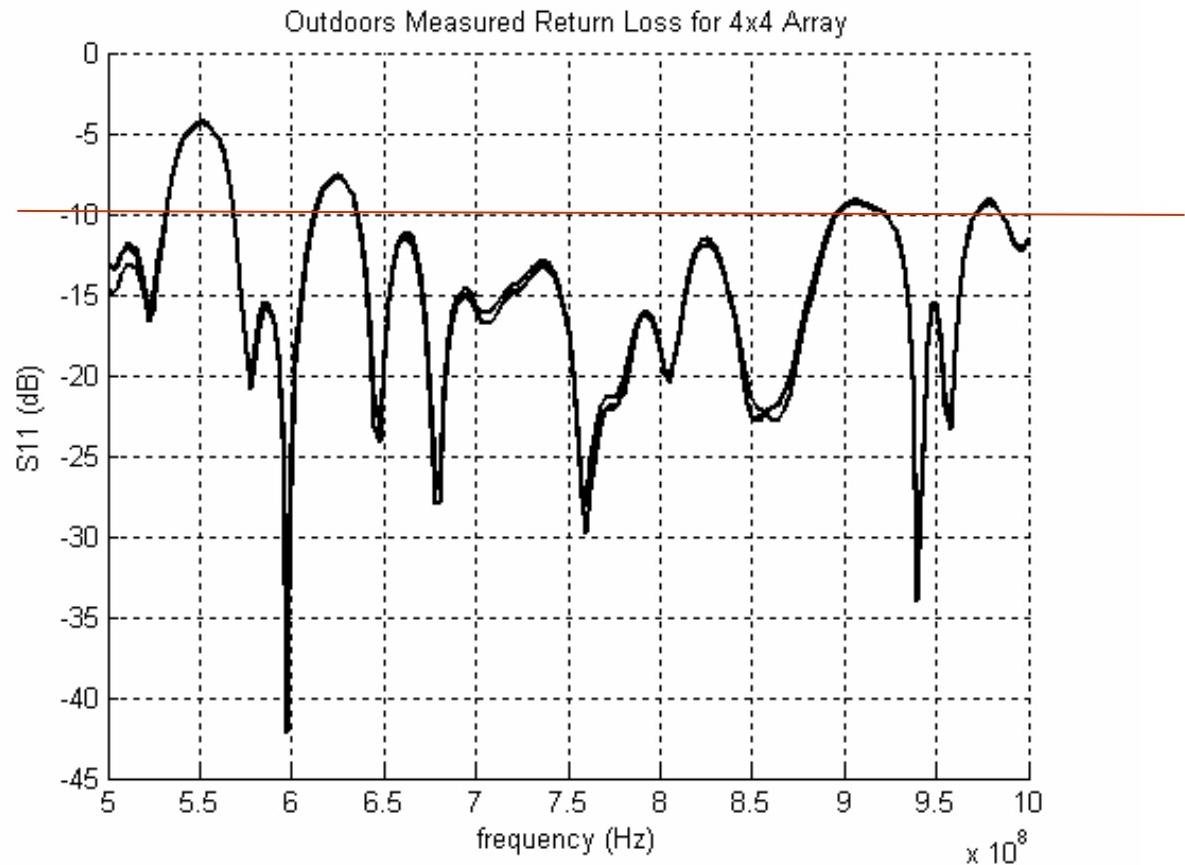
Optimized Power Dividers

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- Replacement for conventional Digital TV antennas



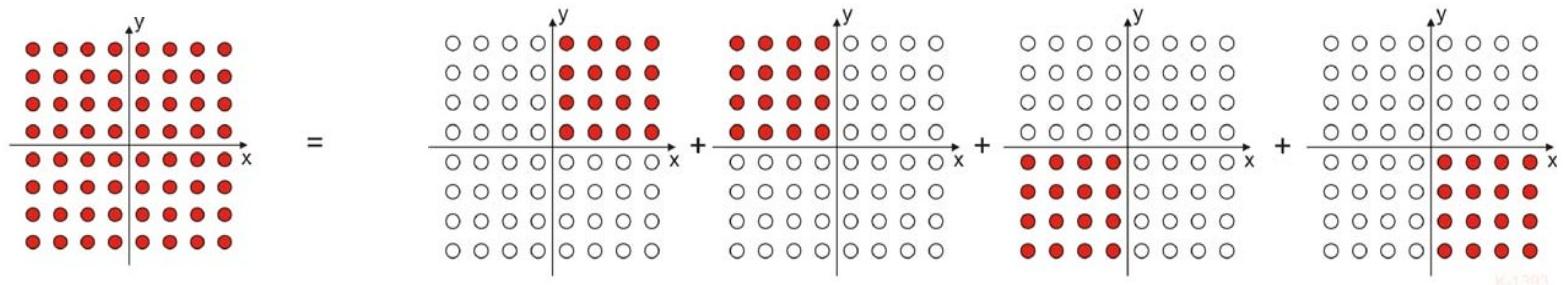
- S_{11} for a 4x4 array of ribcage dipoles
- It can be used for Digital TV reception in the UHF band: 400-900 MHz

- Modeling a **finite 8x8 antenna array** of ribcage dipoles with balun in Ansoft HFSS requires
 - ~ 21 hours
 - 70 GB of memory on a
 - 64-bit Windows machine
- We have developed a simplified methodology that exploits the symmetry of the array and array excitations
- We have implemented an algorithm that allows to compute the total field pattern for the 8x8 antenna array from the analysis of one 6x6 sub-array
- Modeling a **finite 6x6 sub-array** of ribcage dipoles with balun in Ansoft HFSS requires
 - ~ 6 hours
 - 20 GB of memory on a
 - 64-bit Windows machine

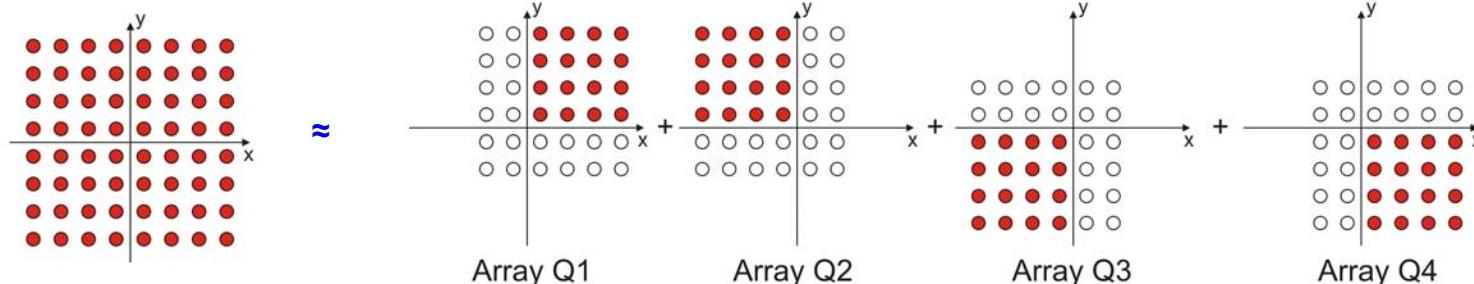
Simplified Composite Array Model

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- The total array field pattern can be expressed as superposition of four array field patterns, when the quadrants Q1, Q2, Q3, and Q4 are excited
- Only 16 elements are excited at any one time, while the remaining elements are passive and match-terminated (50Ω)

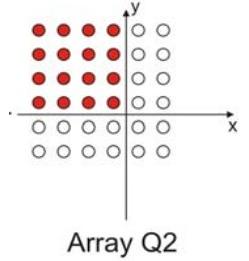
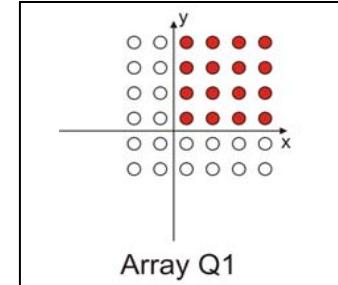


- Approximation: truncate the passive arrays by removing the two outermost rows and columns.
- Now there are four 6x6 arrays, which can be analyzed/simulated separately



- When the array excitation is symmetric with respect to the x- and y-axes:

$$\bar{E}_{Q3}(\theta, \varphi) = -\bar{E}_{Q1}(\theta, \varphi)$$



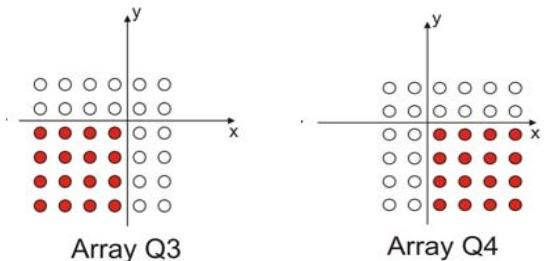
- Q2 and Q4 are mirror images of Q1 and Q3:

$$\bar{E}_{Q2,\theta}(\theta, \varphi) = -\bar{E}_{Q1,\theta}(\theta, \pi - \varphi)$$

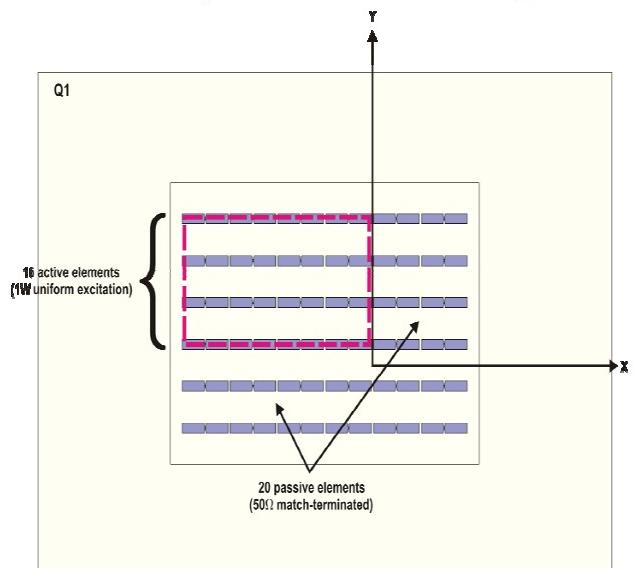
$$\bar{E}_{Q2,\varphi}(\theta, \varphi) = \bar{E}_{Q1,\varphi}(\theta, \pi - \varphi)$$

$$\bar{E}_{Q4,\theta}(\theta, \varphi) = \bar{E}_{Q1,\theta}(\theta, -\varphi)$$

$$\bar{E}_{Q4,\varphi}(\theta, \varphi) = -\bar{E}_{Q1,\varphi}(\theta, -\varphi)$$

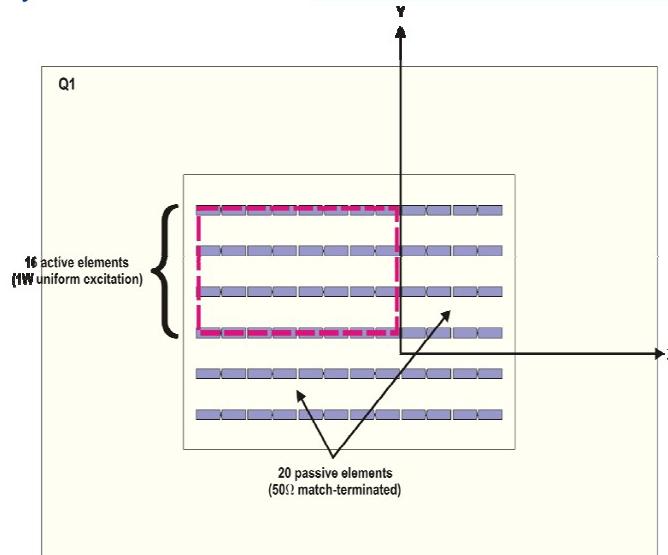


- A highly accurate representation for the far field of the 8x8 array can be obtained from the computation of a single 6x6 array (Q1)

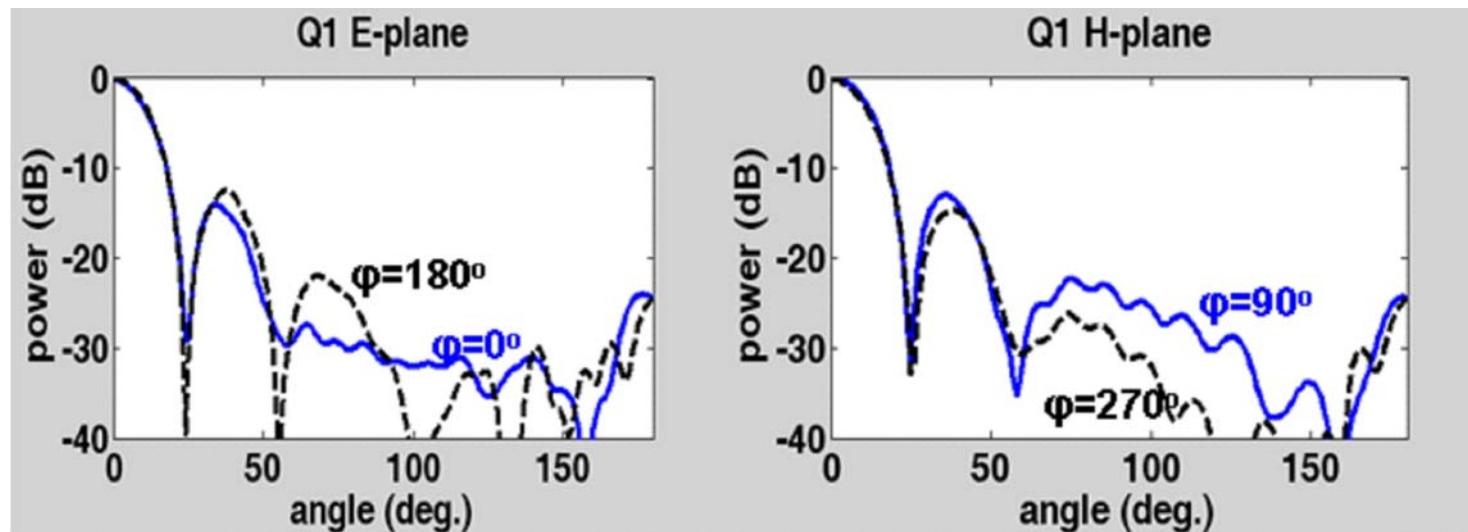


Q1 Sub-Array Pattern

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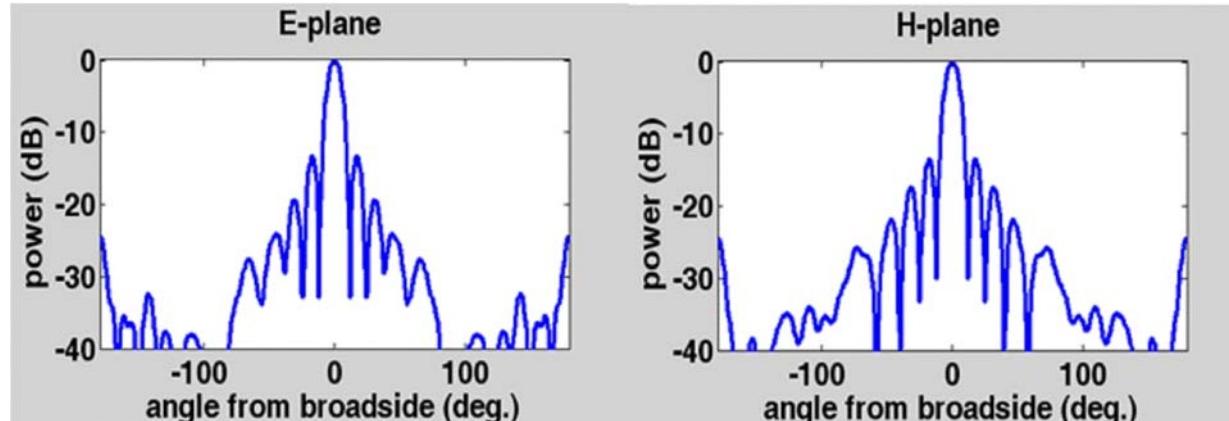
**Q1 sub-array pattern at 750 MHz:
E-plane and H-plane**



8x8 array Gain From Simplified Composite Array Model

The array directivity D is obtained by simple integration:

$$D = \frac{|E_{\max}|^2}{\iint |E_{\max}|^2 \sin \theta d\theta d\varphi}$$



Frequency	Aperture Gain	Gain Computed from Composite Array Model	Total Gain (array gain - net loss in feeding network)
500 MHz	21.1 dB	21.5 dB	19.0 dB
750 MHz	24.6 dB	24.7 dB	22.2 dB
1000 MHz	27.1 dB	26.4 dB	23.9 dB

Conclusions

- **Wideband ribcage dipole as a single radiator:**
 - Combines advantages of blade dipole and droopy dipole
 - Achieves wide impedance bandwidth up to 3.2:1 while maintaining good pattern stability
 - Has low profile when mounted parallel to a ground or air vehicle
- **Array of ribcage elements:**
 - Has performance similar to a parabolic antenna while occupying less volume (e.g. 3 m diameter vs 1.92x1.92 m)
 - Can be stowed and transported in smaller sub-array modules (e.g. four 4x4 sub-arrays for an 8x8 array)
 - Its gain pattern was computed using a Simplified Composite Array Model

Acknowledgement

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This material is based upon work supported by the United States Army under Contract Number W15QKN-08-C-0493. Any opinions, findings and conclusions or recommendations expressed in this material are those of the author(s) and do not necessarily reflect the views of the United States Army.